



UNIVERSITY OF
ILLINOIS
URBANA - CHAMPAIGN

ME 330: Engineering Materials

Lab - 2

Uniaxial Tension Tests



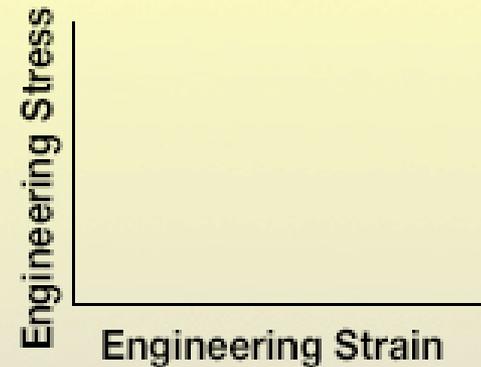
**Grainger College
of Engineering**

UNIVERSITY OF ILLINOIS URBANA-CHAMPAIGN

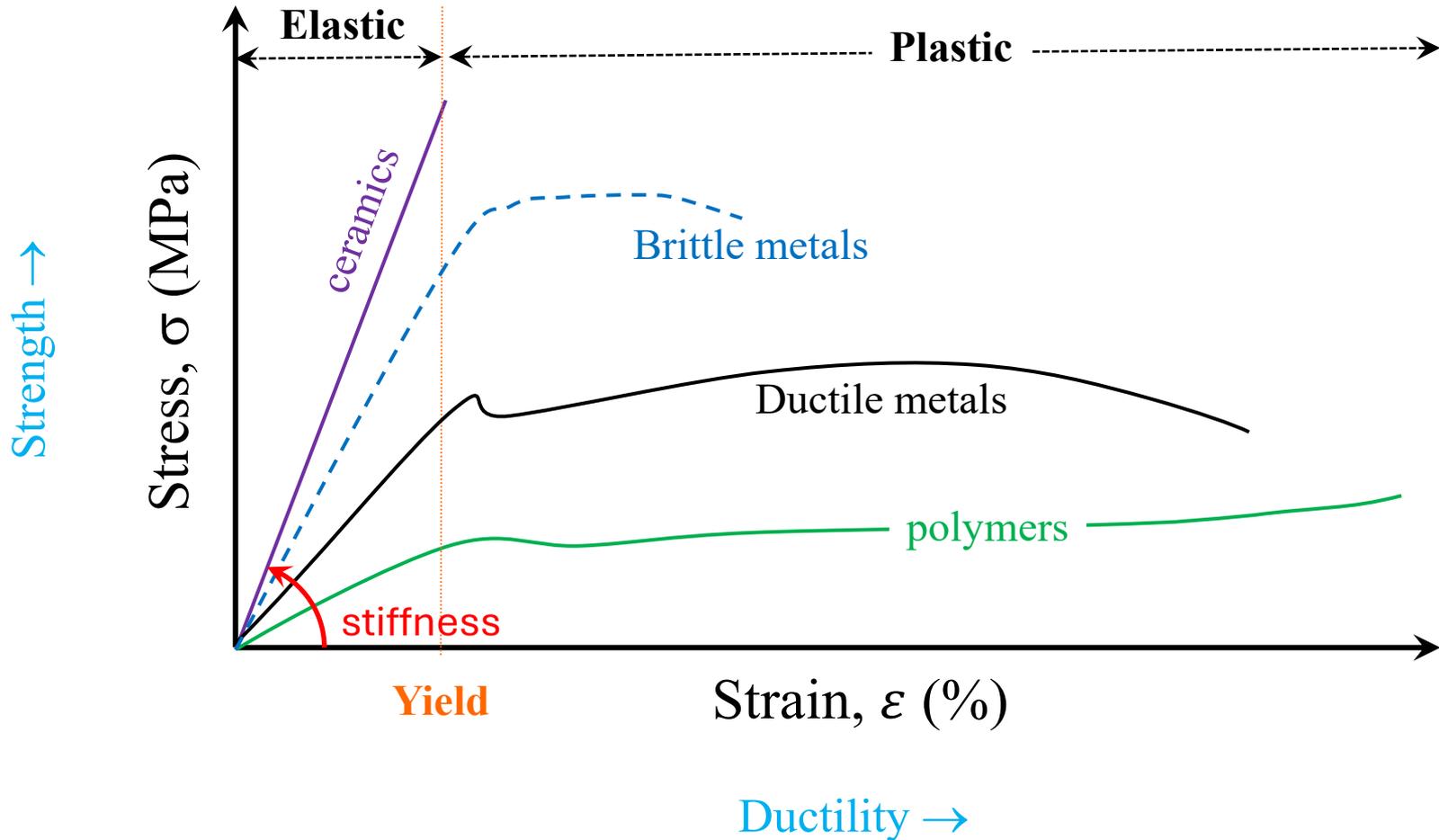
Tensile Test

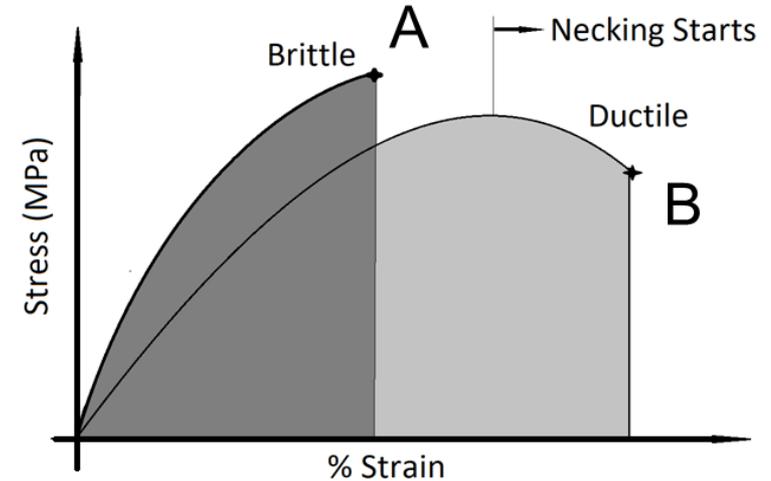
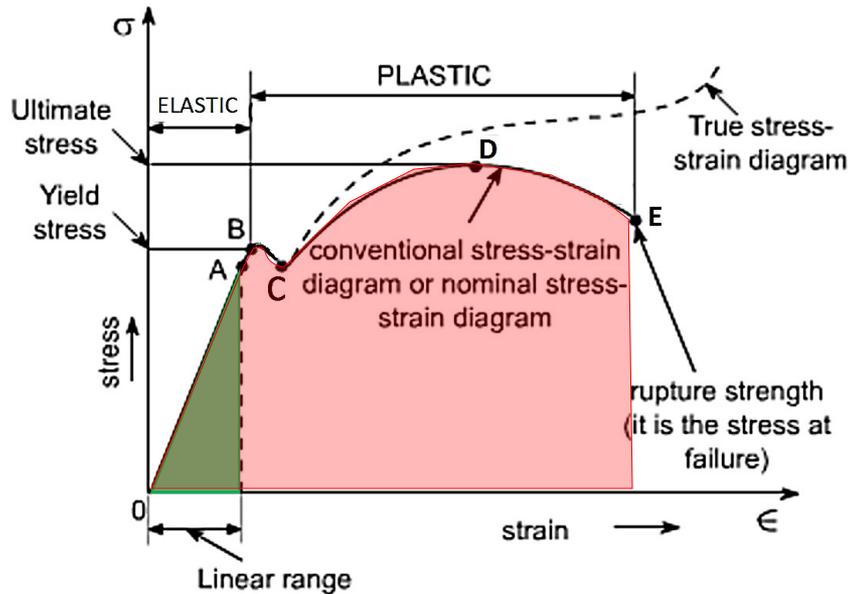
1. Cast Iron (demo)
2. Steel 1045
Cold Rolled,
Normalized
3. Aluminum
2024-T4,
7075-T6
4. Stainless Steel
5. PMMA
6. Brass(demo)

Tensile Test Steel



Typical Stress-Strain Curves





Engineering stress : $\sigma = F/A_0$

Engineering strain : $\epsilon = (L_i - L_0)/L_0$

True stress : $\sigma_T = F/A_i$

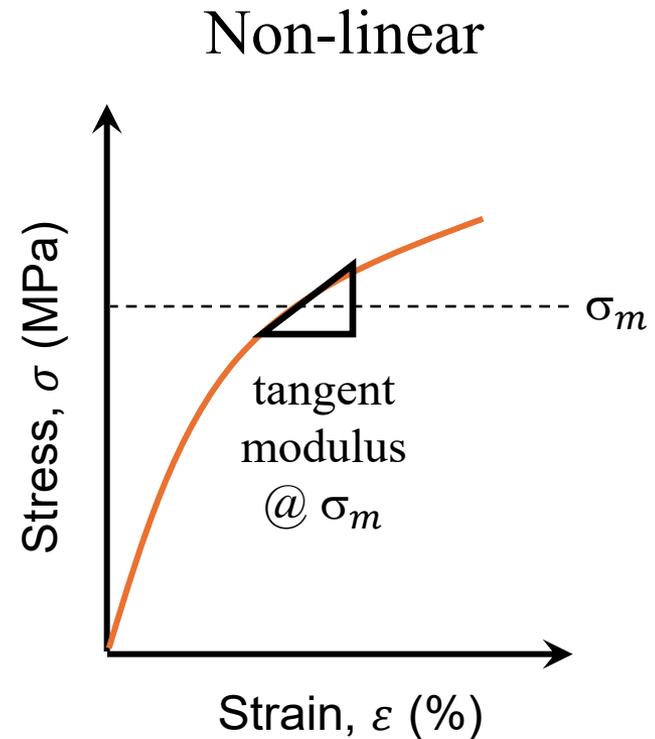
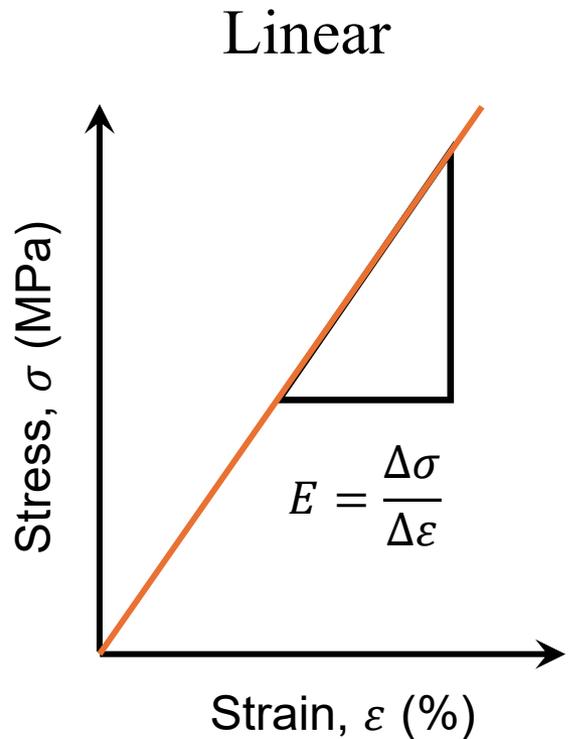
True strain : $\epsilon_T = \ln(L_i/L_0)$

$$\sigma_T = \sigma(\epsilon + 1)$$

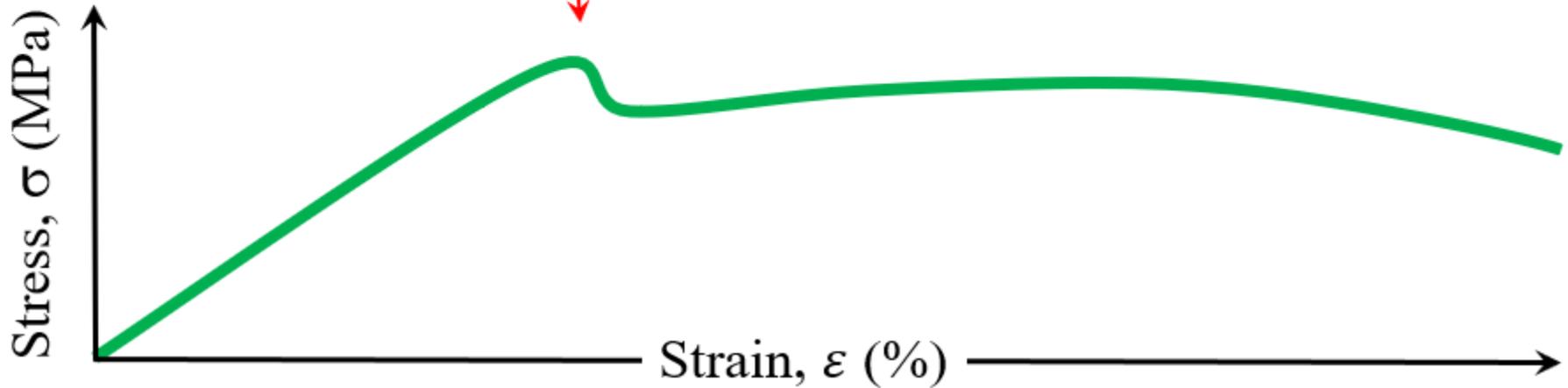
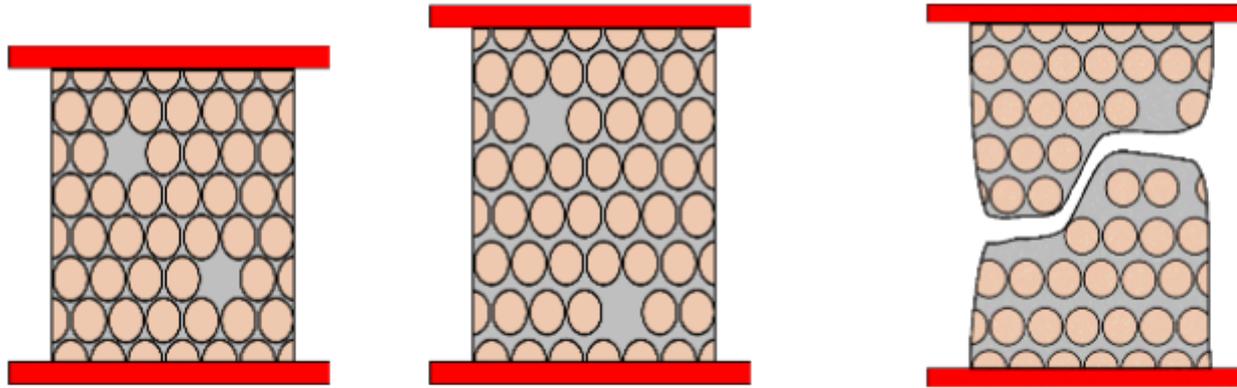
$$\epsilon_T = \ln(\epsilon + 1)$$

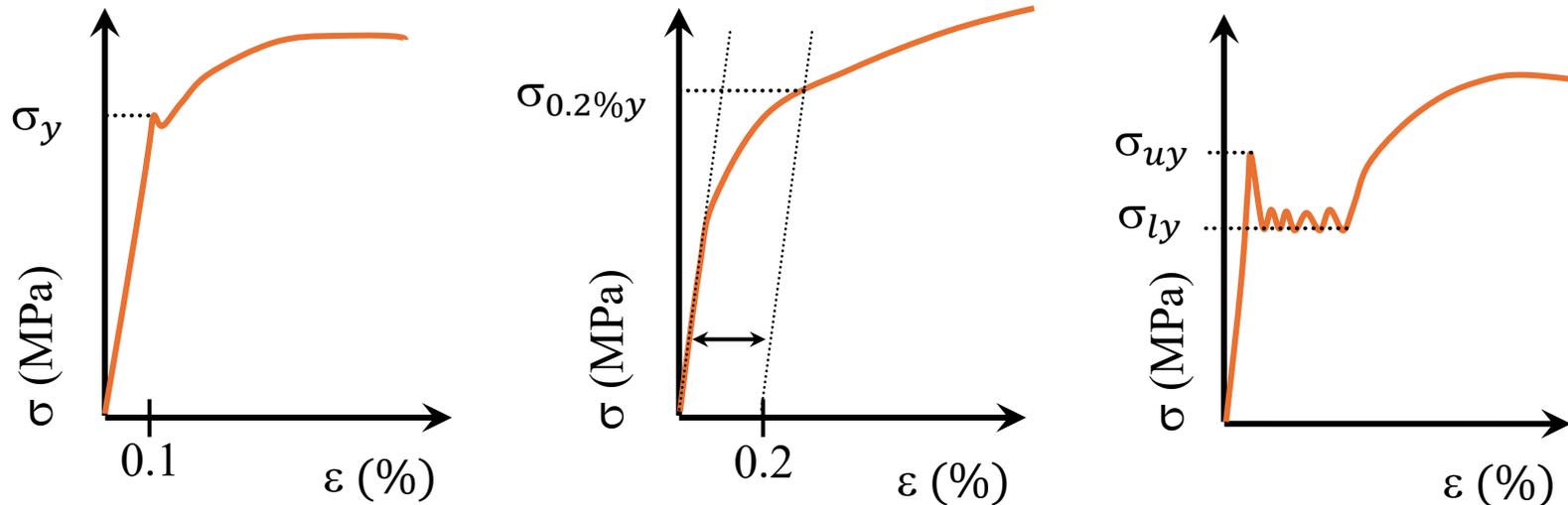
- ❖ Value on curve:
 - What material is stronger?
 - What material is ductile?
- ❖ Initial slope of curve:
 - What material is stiffer?
- ❖ Area under curve:
 - What material is more resilient?
 - What material is tougher?
 - What material is better for shock absorption?
- ❖ Hardness ????????

- Elastic region: strain returns to zero when stress removed (100 % reversible)
- Elastic Modulus (E) - measure of stiffness

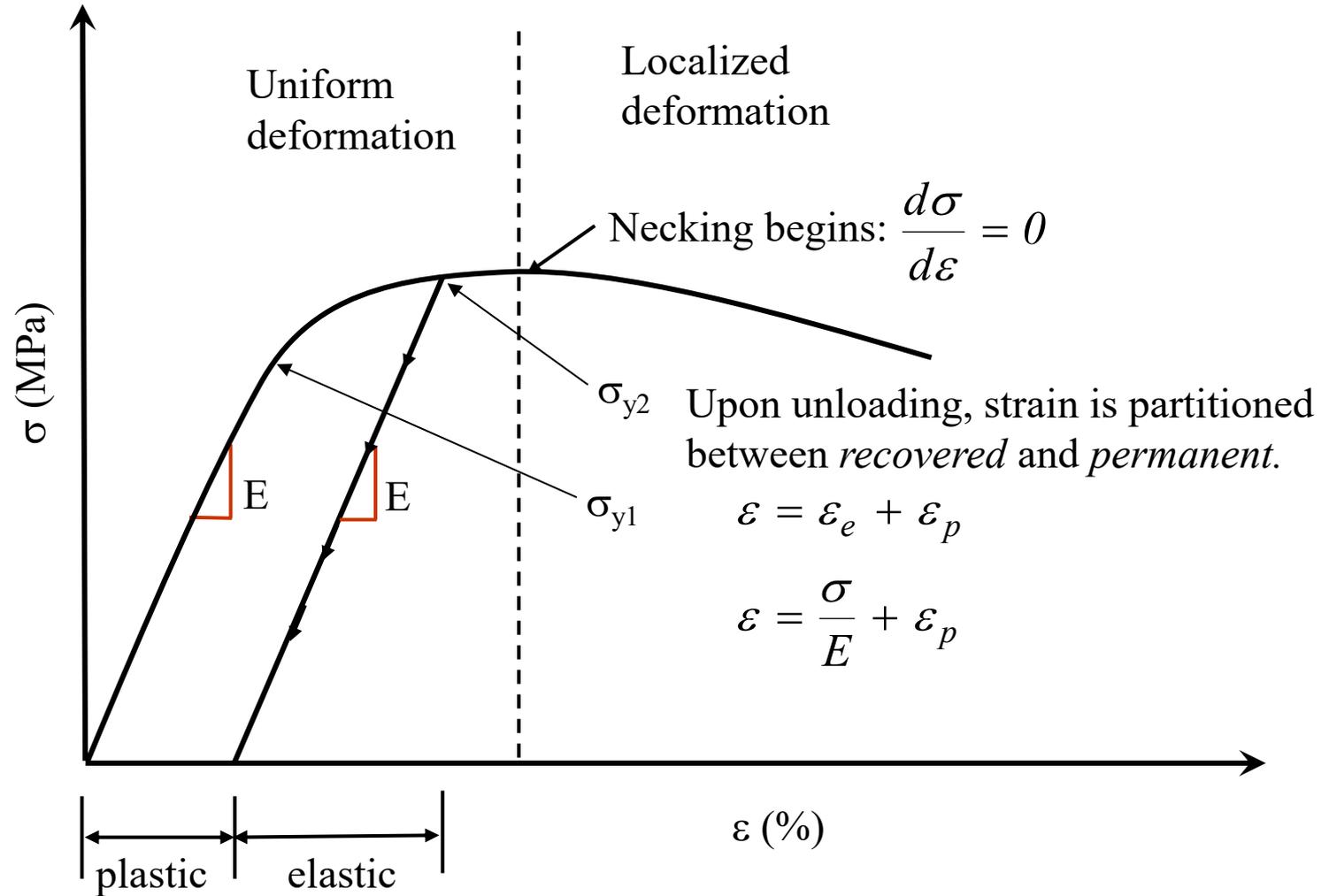


Yielding



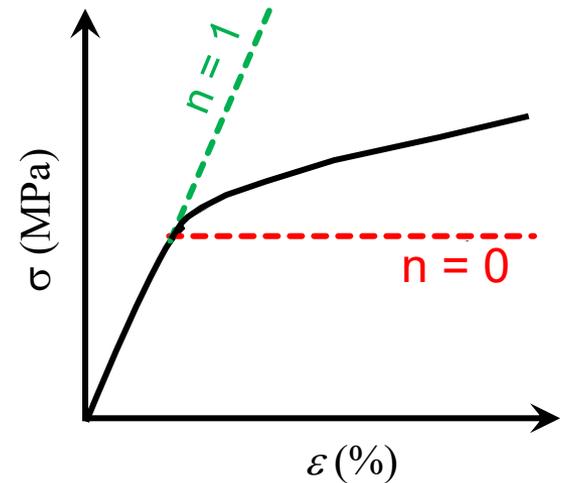


- **Proportional limit** marks the end of linearity
- **Yield point** marks the beginning of plastic deformation
 - Some materials show an obvious transition, σ_y
 - Often need to define 0.2% offset yield, $\sigma_{0.2\%y}$
 - Sometime see an upper (σ_{uy}) and lower (σ_{ly}) yield stresses occur
 - Caused by significant dislocation-solute interaction
 - Common in BCC iron-based alloys



- Can approximate relation between true stress-strain curve in *constant plastic deformation* region by:

$$\sigma_t = K \varepsilon_t^n$$



- K is the strength parameter ?
- n is the strain-hardening exponent ($0 \leq n < 1$)
 - if $n = 0$, elastic-perfectly plastic response
 - if $n = 1$, ideally elastic material
 - as n increases, achieve more strain hardening
- Typically, valid only for some metals and alloys
- Termed “power law hardening”

Percent Elongation:

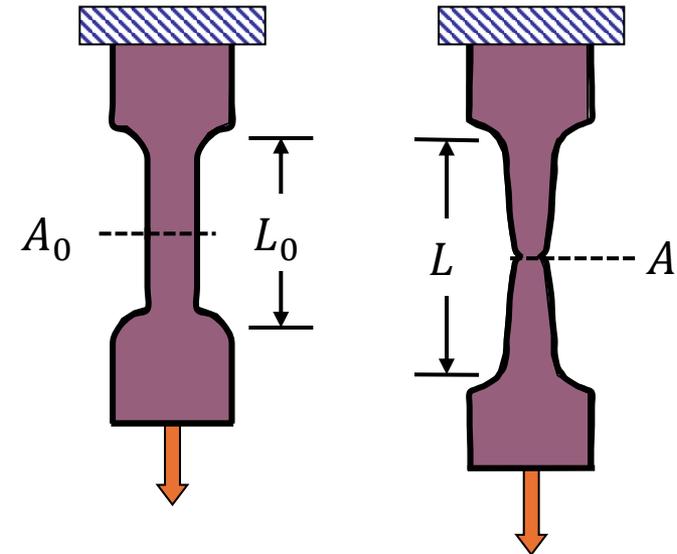
$$\%EL = \left(\frac{L - L_0}{L_0} \right) \times 100\%$$

Sensitive to gage length
Does not account for necking

Area reduction:

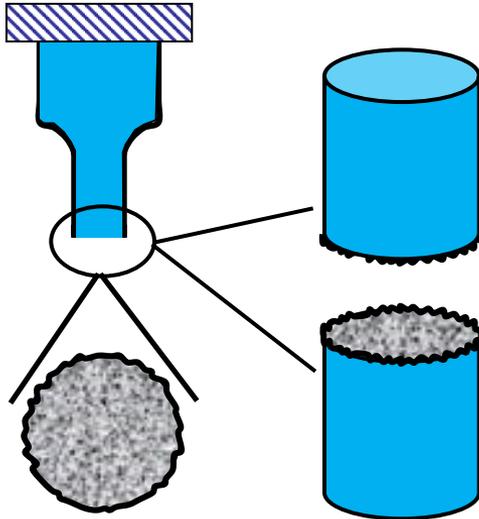
$$\%AR = \left(\frac{A_0 - A}{A_0} \right) \times 100\%$$

Insensitive to gage length
Does account for necking
Sensitive to cross-section



Fracture Surfaces

Brittle

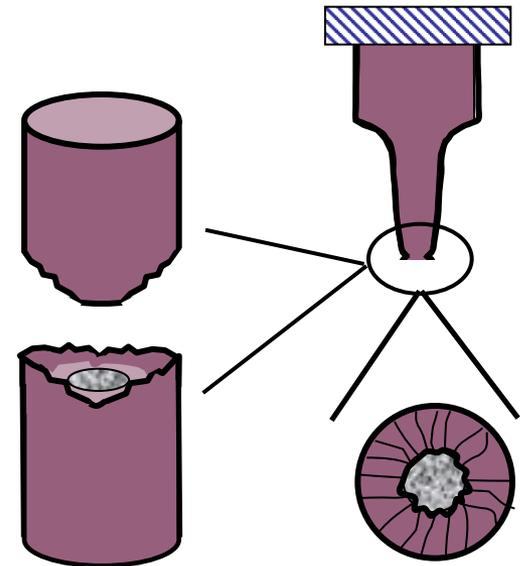


- Cleavage failure
- Flat, rough fracture surface
- No necking
- Failure in tension

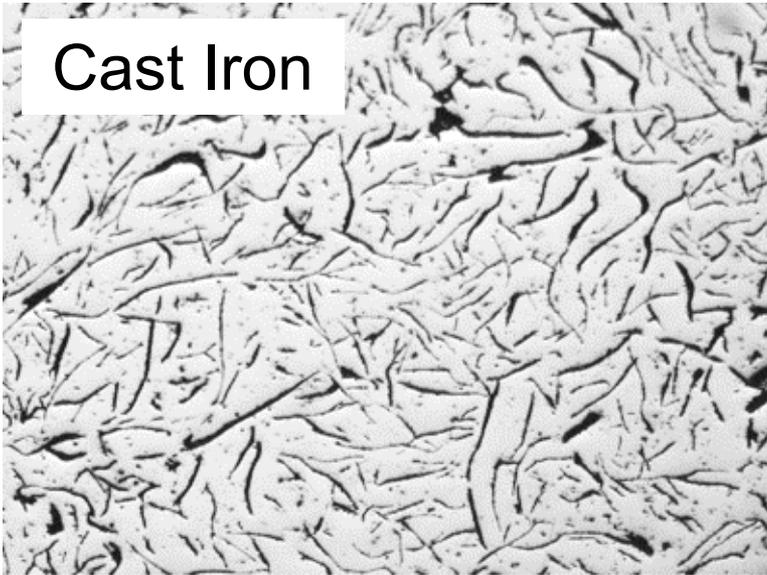
- Completely ductile failure necks to a point
- Cup-cone fracture surface
 - Necking prior fracture
 - Cavities initiate in neck
 - Voids coalesce to form crack
 - Final failure in shear
- Discuss more completely in fracture



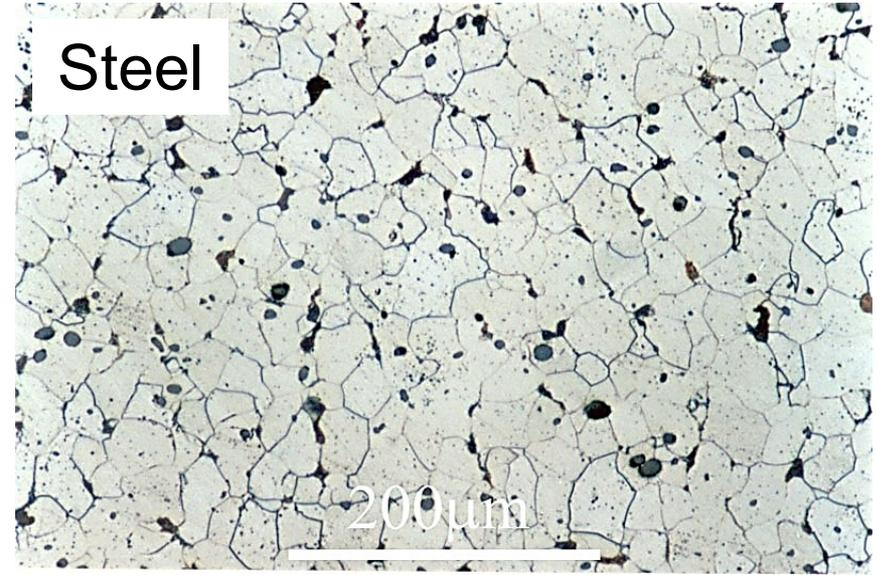
Ductile



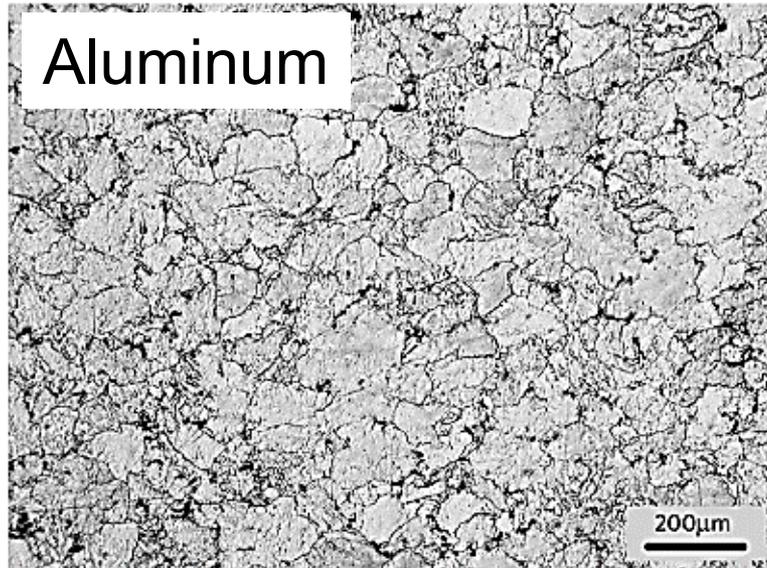
Cast Iron



Steel



Aluminum



Brass

